

# Solving the multi-response problem in Taguchi method by benevolent formulation in DEA

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Received: 9 October 2008 / Accepted: 24 August 2009 / Published online: 16 September 2009  
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**Abstract** The Taguchi method is an efficient approach for optimizing a single quality response. In practice, however, most products/processes have more than one quality response of main interest. Recently, the multi-response problem in the Taguchi method has gained a considerable research attention. This research, therefore, proposes an efficient approach for solving the multi-response problem in the Taguchi method utilizing benevolent formulation in data envelopment analysis (DEA). Each experiment in Taguchi's orthogonal array (OA) is treated as a decision making unit (DMU) with multiple responses set inputs and/or outputs. Each DMU is evaluated by benevolent formulation. The ordinal value of the DUM's efficiency is then used to decide the optimal factor levels for multi-response problem. Three frequently-investigated case studies are adopted to illustrate the proposed approach. The computational results showed that the proposed approach provides the largest total anticipated improvement among principal component analysis (PCA), DEA based ranking approach (DEAR) and other techniques in literature. In conclusion, the proposed approach may provide a great assistant to practitioners for solving the multi-response problem in manufacturing applications on the Taguchi method.

**Keywords** Multi-response problem · Taguchi method · DEA · Benevolent formulation

## Introduction

Failure to select the best condition of process factors is a costly mistake in today's highly competitive markets. The overall goal of robust design is to find settings of the controllable factors so that the response is least sensitive to variations in the noise variables, while still yielding an acceptable mean level of the response. Taguchi (1991) method is a widely used approach for robust design, which utilizes an orthogonal array (OA) to obtain dependable information about the design parameter with minimum time and resources, and adopts signal-to-noise (S/N) ratio to interpret experimental data and optimize performance. Nevertheless, this method is found only efficient for determining the optimal setting of controllable factor levels which optimize a single response problem; such as, flank wear (Tsao and Hocheng 2002), thickness of solder paste (Li et al. 2008) and casting porosity (Anastasiou 2002).

Today's sharp market competition has forced most industries to produce products with more than one response. To solve the multi-response problem, the Taguchi method adopts a trade-off between quality loss and productivity by engineering judgment (Phadke 1989). But, this approach may provide contradictory optimal factor levels for multi-response problem and increases uncertainty in decision-making process. Shiau (1990) assigned a weight for each response then employed the sum of the weighted responses. Tong et al. (1997) used the S/N ratio for the sum of the weighted normalized quality losses. However, it still remains difficult to decide a weight for each quality response in real applications. Reddy et al. (1997) adopted regression techniques-based approaches to optimize the multi-response problem. Unfortunately, regression approaches increase the complexity of computational process and thus require statistical skills. Further, Antony (2000) utilized principal

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component analysis (PCA) to transform the multi-responses in few uncorrelated ones. The principal components were then used to find the optimal factor levels for multi-responses. But, PCA is based on some rigid assumption that the error terms are multivariate normally distributed random variable, which may limit its application in real applications. Furthermore, Yu et al. (2004) proposed a strategy called fuzzy neural-Taguchi network with genetic algorithm, Jeyapaul et al. (2006) deployed genetic algorithm, and Al-Refaie et al. (2008) employed grey analysis for optimizing the multi-response problem in the Taguchi method. In reality, the soft computing techniques genetic algorithm and neural networks, and grey analysis are still not be completely understood by many practitioners.

Data envelopment analysis (DEA) proposed by Charnes et al. (1978) is a fractional mathematical programming technique for evaluating the relative efficiency of homogeneous decision making units (DMUs) with multiple inputs and multiple outputs. DEA combines various inputs and various outputs for a DMU into one performance measure, called relative efficiency. DEA techniques can be divided into two categories. The techniques in the first category incorporate a priori information provided by a decision maker or expert, whereas the techniques in the other category do not incorporate a priori information (Angulo-Meza and Lins 2002). The first category includes direct weight restrictions (Dyson and Thanassoulis 1988), the cone ratio model (Charnes et al. 1990), and value efficiency analysis Halme et al. 2000). However, there are disadvantages in these methods concerning subjectivity. First, the priori information can be wrong or biased. Second, there may be a lack of consensus among the experts or decision-makers, which may adversely affect the study. In contrast, the techniques in the second category do not rely on priori information, provide reliable conclusions, and consequently, improve the decision making process. Among the techniques in the second category is benevolent formulation in cross-evaluation. Unlike the traditional DEA techniques, benevolent formulation increases discrimination among efficient DMUs and allows for DMU's peer-evaluation instead of self-evaluation. To utilize these advantages and reduce the uncertainty in the decision making process, this research employs benevolent formulation for solving the multi-response in the Taguchi method. Each experiment of Taguchi's array is treated as a DMU with multi-responses set as inputs and/or outputs. Benevolent formulation is then used to evaluate performance for each DMU and decide optimal factor levels for multi-responses. The remainder of this paper is organized as follows. DEA is introduced in "Data envelopment analysis". The proposed approach is presented in "The proposed approach". The application of the proposed approach is illustrated in "Application of the proposed approach". Conclusions are finally summarized in the last section.

## Data envelopment analysis

Data envelopment analysis has been widely used for evaluating performance for a set of DMUs with multiple inputs and multiple outputs at organizational level, such as banks, hospitals, and universities (Charnes et al. 1994). The widely-used DEA technique is the CCR model, which is developed by Charnes et al. (1978).

### The CCR model

The CCR model displayed in "Appendix A" measures the relative efficiency of each DMU once by comparing it to a group of the other DMUs that have the same set of inputs and outputs. Let  $DMU_o$  denotes a DMU to be evaluated. Then,  $DMU_o$  is identified as CCR-efficient if its relative efficiency,  $E_o$ , equals one. Otherwise, it is identified as inefficient. However, the CCR model fails to discriminate among efficient DMUs, since the relative efficiency scores may be equal to one for more than one DMU. On the other hand, Khouja (1995) adopted two phases approach in the selection of advanced manufacturing technology (robots) from a list of feasible technologies. In the first phase, the robot efficiencies are identified by the CCR model then evaluated by a multi-attribute decision-making model in the second phase. Liao (2005) used neural networks to predict the responses for all factor level combinations. The CCR model is then employed to decided optimal factor settings. However, Baker and Talluri (1997) investigated the robot selection problem in Khouja's study and showed that CCR model has an intrinsic problem that provides misleading efficiency scores through identifying a DMU with an unrealistic weighing scheme to be efficient. In addition, it may result in multiple optimal solutions. To avoid the above shortcoming of CCR model, this research utilizes the benevolent formulation in cross-evaluation to measure and compare performance of a set of DMUs.

### Benevolent formulation in cross-evaluation

The cross-evaluation technique, initially introduced by Sexton et al. (1986), uses DEA in a peer-evaluation instead of a self-evaluation calculated by CCR model. A self-evaluation is to measure  $DMU_o$ 's efficiency is calculated using its own input and output weights. Whereas, a peer-evaluation means that  $DMU_o$  is evaluated according to the optimal weighting scheme of other DMUs. The mean of these efficiencies is the cross-evaluation. However, multiple optimal solutions can exist, which cause the cross-efficiencies to vary. This problem is solved by introducing a secondary objective function using benevolent formulation. The main idea of benevolent formulation is to obtain a weighing scheme of  $DMU_o$  that would be optimal in CCR model, but have, as a secondary

objective, maximization of the cross-efficiencies of the other DMUs (Angulo-Meza and Lins 2002). This technique can be expressed by two models I and II shown in “Appendix B”. By either model, once the optimal  $u_{ro}$  and  $v_{io}$  values, or  $u_{ro}^*$  and  $v_{io}^*$  respectively, are obtained, the cross-efficiencies of  $DMU_o$  can be calculated. Let  $E_{oj}$  denotes the cross-efficiency of  $DMU_j$  calculated according to the optimal weights of  $DMU_o$ . The  $E_{oj}$  is calculated as:

$$E_{oj} = \frac{\sum_{r=1}^s u_{ro}^* y_{rj}}{\sum_{i=1}^m v_{io}^* x_{ij}} \quad j \neq o. \tag{1}$$

Once the  $E_{oj}$  values are calculated, a matrix called the “cross-efficiencies matrix” is constructed. Let  $e_j$  be the mean of cross-efficiencies for  $DMU_j$  estimated as:

$$e_j = \sum_{o \neq j} E_{oj} / (n - 1) \quad j = 1, \dots, n. \tag{2}$$

The  $e_j$  values are then used for comparing performance of  $n$  DMUs. Unlike the CCR model, the benevolent formulation increases discrimination among efficient DMUs by allowing efficiency takes a value greater than one. Benevolent formulation models are employed for solving the multi-response problem in the Taguchi method as described in the following section.

### The proposed approach

Products have quality responses that describe their performance relative to customer requirements or expectations. Generally, a process/product quality characteristic (QCH) or response is divided into three main types: the smaller-the-better (STB), the nominal-the-best (NTB), and the larger-the-better (LTB) responses. The STB response has an ideal target of zero, such as electromagnetic radiations from telecommunications equipment and leakage current in integrated circuits. The NTB characteristic has a specific user-defined target value, such as the output voltage supply of television. Finally, the LTB response has an ideal state or target of infinity, such as the mechanical strength of a wire per unit cross-section area. In practice, the multi-responses of a product/process are not necessarily belonging to the same response type. In this research, it is assumed that the responses are uncorrelated. In these regards, the proposed approach for solving the multi-response problem in the Taguchi method is outlined in the following steps:

**Step 1** Assume  $n$  experiments are conducted utilizing Taguchi’s OA. Treat each experiment as a DMU. As mentioned earlier, the relative efficiency is defined as the sum of weighted outputs divided by the sum of the weighted inputs. Typically, higher efficiency indi-

cates better performance, which can be achieved if the sum of the weighted outputs increases and/or the sum of the weighted inputs decreases. To enhance the relative efficiency of each DMU and achieve the desired target of each quality response, set the input and output of each DMU as follows:

- (i) If all responses are STB type, then set all responses as inputs, whereas set a unit (one) as the output. Conversely, if all responses are LTB type, set all responses as outputs, while set a unit (one) as the input for all DMUs. In other words, the efficiency is improved by decreasing the denominator in the former case, or increasing the numerator in latter case.
- (ii) If all responses are NTB type, then calculate the quality loss,  $L_j$ , for  $DMU_j$  as follows (Tong et al. 1997):

$$L_j = c(s_j^2/\bar{y}_j^2) \quad j = 1, \dots, n \tag{3}$$

where  $c$  is the quality loss coefficient, while  $\bar{y}_j$  and  $s_j$  are the average and standard deviation of response replicates for of  $DMU_j$ , respectively. Since the objective is to minimize the quality loss, set the  $L_j$  values as inputs and one as the output for all DMUs.

- (iii) If responses are a mix of the three types, set STB type response and  $L_j$  values of the NTB type response as inputs, whereas set LTB type response(s) as the output for all DMUs.

- Step 2** Evaluate the relative efficiency,  $E_o$ , of each DMU by solving the input-oriented CCR model.
- Step 3** Estimate the optimal input and output weights,  $u_{ro}^*$  and  $v_{io}^*$ , by solving Model I for each  $DMU_o$ . Then, calculate the cross-efficiency,  $E_{oj}$ , scores for each DMU using Eq. (1). Construct the cross-efficiencies matrix. Then obtain the average,  $e_j$ , of cross-efficiencies using Eq. (2).
- Step 4** In order to optimize performance, and avoid the bias produced by large  $e_j$  values in selecting optimal levels, decide the ordinal value of  $e_j$ ; the ordinal value is to rank the  $e_j$  values such that the smallest  $e_j$  value receives an ordinal value of one, whereas the largest  $e_j$  value takes an ordinal value of  $n$ . Let  $AOV_{fl}$  be the average of the ordinal values for level  $l$  of factor  $f$ . Calculate the  $AOV_{fl}$  value for each factor level. Typically, higher  $AOV_{fl}$  implies better performance. Therefore, the optimal factor level,  $l^*$ , is identified as the level that maximizes the value of  $AOV_{fl}$ . Mathematically,

$$l^* = \left\{ l \mid \max_l \{AOV_{fl}\} \right\} \quad \forall f \tag{4}$$

If a tie occurs in selecting the optimal level for a factor, choose the factor level that provides the largest anticipated improvement as the optimal level for that factor.

- Step 5 Repeat steps 3 and 4 to evaluate the performance of each DMU using model II instead of Model I.
- Step 6 Estimate the anticipated improvement in each response due to setting factors at optimal levels. Then, compare the anticipated improvement by the proposed approach for each response with the anticipated improvements gained by adopting other approaches in previous studies. If the response have different quality loss coefficients, then calculate the reduction of quality loss in each response. Otherwise, calculate the S/N ratio for each response using

$$S/N \text{ ratio} = -10 \log_{10} \left( \frac{1}{K} \sum_{k=1}^K y_k^2 \right) \text{ for STB type response} \quad (5)$$

$$S/N \text{ ratio} = 10 \log_{10} \frac{\mu^2}{\sigma^2} \text{ for NTB type response} \quad (6)$$

$$S/N \text{ ratio} = -10 \log_{10} \left( \frac{1}{K} \sum_{k=1}^K \frac{1}{y_k^2} \right) \text{ for LTB type response} \quad (7)$$

where  $K$  is the number of response replicates. The  $\mu$  and  $\sigma$  are response mean and standard deviation, respectively. Obtain the average S/N ratio for each factor level.

The following section provides several examples on the application of the proposed approach.

### Application of the proposed approach

Three frequently investigated case studies are selected to illustrate the proposed approach. In the below case studies, the quality loss coefficients for the multiple responses are set equal. Thus, the S/N ratio will be used to estimate the anticipated improvement in each response.

#### Optimizing polysilicon deposition process

Phadke (1989) conducted the Taguchi method to improve the quality of polysilicon process for three responses; the surface

**Table 1** Experimental data of polysilicon process

| DMU <sub>j</sub>  | Control factor <sup>a</sup> |   |   |   |   |   |   | Inputs   |                                        | Output                       | Standard efficiency ( $E_o$ ) |                              |
|-------------------|-----------------------------|---|---|---|---|---|---|----------|----------------------------------------|------------------------------|-------------------------------|------------------------------|
|                   | <i>e</i>                    | A | B | C | D | E | F | <i>e</i> | Quality loss of thickness ( $x_{1j}$ ) | Surface defects ( $x_{2j}$ ) |                               | Deposition rate ( $y_{1j}$ ) |
| DMU <sub>1</sub>  | 1                           | 1 | 1 | 1 | 1 | 1 | 1 | 1        | 0.00030                                | 0.67                         | 14.5                          | 1.00000                      |
| DMU <sub>2</sub>  | 1                           | 1 | 2 | 2 | 2 | 2 | 2 | 2        | 0.00027                                | 36.22                        | 36.6                          | 0.38025                      |
| DMU <sub>3</sub>  | 1                           | 1 | 3 | 3 | 3 | 3 | 3 | 3        | 0.00025                                | 135.78                       | 41.4                          | 0.22037                      |
| DMU <sub>4</sub>  | 1                           | 2 | 1 | 1 | 2 | 2 | 3 | 3        | 0.00006                                | 17.00                        | 36.1                          | 1.00000                      |
| DMU <sub>5</sub>  | 1                           | 2 | 2 | 2 | 3 | 3 | 1 | 1        | 0.00719                                | 1,087.78                     | 73.0                          | 0.02626                      |
| DMU <sub>6</sub>  | 1                           | 2 | 3 | 3 | 1 | 1 | 2 | 2        | 0.00051                                | 839.89                       | 49.5                          | 0.09788                      |
| DMU <sub>7</sub>  | 1                           | 3 | 1 | 2 | 1 | 3 | 2 | 3        | 0.00726                                | 776.33                       | 76.6                          | 0.03359                      |
| DMU <sub>8</sub>  | 1                           | 3 | 2 | 3 | 2 | 1 | 3 | 1        | 0.00520                                | 2,065.33                     | 105.4                         | 0.03032                      |
| DMU <sub>9</sub>  | 1                           | 3 | 3 | 1 | 3 | 2 | 1 | 2        | 0.00087                                | 2,200                        | 115.0                         | 0.13343                      |
| DMU <sub>10</sub> | 2                           | 1 | 1 | 3 | 3 | 2 | 2 | 1        | 0.00206                                | 0.89                         | 24.8                          | 1.00000                      |
| DMU <sub>11</sub> | 2                           | 1 | 2 | 1 | 1 | 3 | 3 | 2        | 0.00013                                | 1.00                         | 20.0                          | 1.00000                      |
| DMU <sub>12</sub> | 2                           | 1 | 3 | 2 | 2 | 1 | 1 | 3        | 0.00016                                | 246.56                       | 39.0                          | 0.25200                      |
| DMU <sub>13</sub> | 2                           | 2 | 1 | 2 | 3 | 1 | 3 | 2        | 0.00062                                | 150.11                       | 53.1                          | 0.16001                      |
| DMU <sub>14</sub> | 2                           | 2 | 2 | 3 | 1 | 2 | 1 | 3        | 0.00005                                | 44.44                        | 45.7                          | 1.00000                      |
| DMU <sub>15</sub> | 2                           | 2 | 3 | 1 | 2 | 3 | 2 | 1        | 0.00018                                | 1,359.44                     | 54.8                          | 0.30722                      |
| DMU <sub>16</sub> | 2                           | 3 | 1 | 3 | 2 | 3 | 1 | 2        | 0.00065                                | 14.33                        | 76.8                          | 0.67157                      |
| DMU <sub>17</sub> | 2                           | 3 | 2 | 1 | 3 | 1 | 2 | 3        | 0.00629                                | 2,201.22                     | 105.3                         | 0.02609                      |
| DMU <sub>18</sub> | 2                           | 3 | 3 | 2 | 1 | 2 | 3 | 1        | 0.01438                                | 3,333.33                     | 91.4                          | 0.01227                      |

<sup>a</sup> *e* Indicates empty column

**Table 2** The S/N ratio averages for polysilicon process

| Response (dB)   | Level <sup>a</sup> | Factor        |               |               |               |               |               | Optimal factor levels using Taguchi method                                                | Overall average (dB) |
|-----------------|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|-------------------------------------------------------------------------------------------|----------------------|
|                 |                    | A             | B             | C             | D             | E             | F             |                                                                                           |                      |
| Thickness       | 1                  | <b>35.12</b>  | 31.61         | <b>34.39</b>  | 31.68         | 30.52         | 27.04         | A <sub>1</sub> B <sub>3</sub> C <sub>1</sub> D <sub>2</sub> E <sub>2</sub> F <sub>3</sub> | 31.52                |
|                 | 2                  | 34.91         | 30.70         | 27.86         | <b>34.70</b>  | <b>32.87</b>  | 33.67         |                                                                                           |                      |
|                 | 3                  | 24.52         | <b>32.24</b>  | 32.30         | 28.16         | 31.16         | <b>33.85</b>  |                                                                                           |                      |
| Surface defects | 1                  | <b>-24.23</b> | <b>-27.55</b> | <b>-39.03</b> | <b>-39.20</b> | -51.53        | -45.56        | A <sub>1</sub> B <sub>1</sub> C <sub>1</sub> D <sub>1</sub> E <sub>2</sub> F <sub>2</sub> | -45.36               |
|                 | 2                  | -50.11        | -47.44        | -55.99        | -46.85        | <b>-40.54</b> | <b>-41.58</b> |                                                                                           |                      |
|                 | 3                  | -61.76        | -61.10        | -41.07        | -50.04        | -44.03        | -48.95        |                                                                                           |                      |
| Deposition rate | 1                  | 28.76         | 32.03         | 32.80         | 32.21         | 34.06         | 33.81         | A <sub>3</sub> B <sub>3</sub> C <sub>2</sub> D <sub>3</sub> E <sub>3</sub> F <sub>3</sub> | 34.12                |
|                 | 2                  | 34.13         | 34.78         | <b>35.29</b>  | 34.53         | 33.99         | 34.10         |                                                                                           |                      |
|                 | 3                  | <b>39.46</b>  | <b>35.54</b>  | 34.25         | <b>35.61</b>  | <b>34.30</b>  | <b>34.44</b>  |                                                                                           |                      |

<sup>a</sup> Optimal levels using Taguchi method for each response are identified by bold type

**Table 3** The optimal DMU weights using benevolent formulation for polysilicon process

| DMU <sub>j</sub>  | Model I   |                              |                              |                                                    | Model II  |                              |                              |                                                    |
|-------------------|-----------|------------------------------|------------------------------|----------------------------------------------------|-----------|------------------------------|------------------------------|----------------------------------------------------|
|                   | δ         | Optimal input weights        |                              | Optimal output weight u <sub>1j</sub> <sup>*</sup> | δ         | Optimal input weights        |                              | Optimal output weight u <sub>1j</sub> <sup>*</sup> |
|                   |           | v <sub>1j</sub> <sup>*</sup> | v <sub>2j</sub> <sup>*</sup> |                                                    |           | v <sub>1j</sub> <sup>*</sup> | v <sub>2j</sub> <sup>*</sup> |                                                    |
| DMU <sub>1</sub>  | 0.0327186 | 21.6778700                   | 0.0000000                    | 0.0004485                                          | 0.0327186 | 21.6778700                   | 0.0000000                    | 0.0004485                                          |
| DMU <sub>2</sub>  | 0.0016940 | 21.6637800                   | 0.0000000                    | 0.0000608                                          | 0.0016940 | 21.6637800                   | 0.0000000                    | 0.0000608                                          |
| DMU <sub>3</sub>  | 0.0028646 | 0.0000000                    | 0.0000696                    | 0.0000503                                          | 0.0028646 | 0.0000000                    | 0.0000696                    | 0.0000503                                          |
| DMU <sub>4</sub>  | 0.0005598 | 21.5656700                   | 0.0000000                    | 0.0000358                                          | 0.0005598 | 21.5656700                   | 0.0000000                    | 0.0000358                                          |
| DMU <sub>5</sub>  | 0.0017380 | 25.4842000                   | 0.0000000                    | 0.0000659                                          | 0.0017380 | 25.4842000                   | 0.0000000                    | 0.0000659                                          |
| DMU <sub>6</sub>  | 0.0082819 | 0.0000000                    | 0.0000732                    | 0.0001215                                          | 0.0082819 | 0.0000000                    | 0.0000732                    | 0.0001215                                          |
| DMU <sub>7</sub>  | 0.0024378 | 25.5297400                   | 0.0000000                    | 0.0000813                                          | 0.0024378 | 25.5297400                   | 0.0000000                    | 0.0000813                                          |
| DMU <sub>8</sub>  | 0.0025150 | 0.0000000                    | 0.0000804                    | 0.0000477                                          | 0.0025150 | 0.0000000                    | 0.0000804                    | 0.0000477                                          |
| DMU <sub>9</sub>  | 0.0147606 | 0.0000000                    | 0.0000812                    | 0.0002074                                          | 0.0147606 | 0.0000000                    | 0.0000812                    | 0.0002074                                          |
| DMU <sub>10</sub> | 0.1956822 | 22.5377500                   | 0.0000000                    | 0.0018721                                          | 0.1956822 | 22.5377500                   | 0.0000000                    | 0.0018721                                          |
| DMU <sub>11</sub> | 0.0053359 | 21.5982700                   | 0.0000000                    | 0.0001404                                          | 0.0053359 | 21.5982700                   | 0.0000000                    | 0.0001404                                          |
| DMU <sub>12</sub> | 0.0075734 | 0.0000000                    | 0.0000701                    | 0.0001117                                          | 0.0075734 | 0.0000000                    | 0.0000701                    | 0.0001117                                          |
| DMU <sub>13</sub> | 0.0007723 | 21.8292900                   | 0.0000000                    | 0.0000408                                          | 0.0007723 | 21.8292900                   | 0.0000000                    | 0.0000408                                          |
| DMU <sub>14</sub> | 0.0041721 | 0.0000000                    | 0.0000691                    | 0.0000672                                          | 0.0041721 | 0.0000000                    | 0.0000691                    | 0.0000672                                          |
| DMU <sub>15</sub> | 0.0434181 | 0.0000000                    | 0.0000760                    | 0.0005795                                          | 0.0434181 | 0.0000000                    | 0.0000760                    | 0.0005795                                          |
| DMU <sub>16</sub> | 0.0045817 | 21.8436000                   | 0.0000000                    | 0.0001242                                          | 0.0045817 | 21.8436000                   | 0.0000000                    | 0.0001242                                          |
| DMU <sub>17</sub> | 0.0022387 | 0.0000000                    | 0.0000812                    | 0.0000443                                          | 0.0022387 | 0.0000000                    | 0.0000812                    | 0.0000443                                          |
| DMU <sub>18</sub> | 0.0011926 | 31.2012500                   | 0.0000000                    | 0.0000602                                          | 0.0011926 | 31.2012500                   | 0.0000000                    | 0.0000602                                          |

defects (STB), thickness (NTB, target is 3,600 Å) and deposition rate (LTB) are the main responses. Six process factors were investigated simultaneously including: (A) deposition temperature, (B) deposition pressure, (C) nitrogen flow, (D) silane flow, (E) settling time, and (F) cleaning method, utilizing L<sub>18</sub> (2<sup>1</sup> × 3<sup>7</sup>) array shown in Table 1. The Taguchi method utilizes the S/N ratio to decide the optimal factor levels for each response. Typically, in this method higher S/N ratio indicates better performance. Using the appropriate formula from Eqs. (5) to (7) for each type response, the average

S/N ratio for each factor level is calculated and displayed in Table 2.

From Table 2, the optimal factor levels for thickness, surface defects, and deposition rate are identified as A<sub>1</sub>B<sub>3</sub>C<sub>1</sub>D<sub>2</sub>E<sub>2</sub>F<sub>3</sub>, A<sub>1</sub>B<sub>1</sub>C<sub>1</sub>D<sub>1</sub>E<sub>2</sub>F<sub>2</sub>, and A<sub>3</sub>B<sub>3</sub>C<sub>2</sub>D<sub>3</sub>E<sub>3</sub>F<sub>3</sub>, respectively. Obviously, there exists a conflict among these combinations about the optimal factor levels for optimizing the three responses concurrently. To optimize the three responses concurrently by the proposed approach, the following steps were conducted:

**Table 4** The cross-efficiencies matrix by benevolent formulation model I and II for polysilicon process

| DMU <sub>i</sub>  | DMU <sub>1</sub> | DMU <sub>2</sub> | DMU <sub>3</sub> | DMU <sub>4</sub> | DMU <sub>5</sub> | DMU <sub>6</sub> | DMU <sub>7</sub> | DMU <sub>8</sub> | DMU <sub>9</sub> | DMU <sub>10</sub> | DMU <sub>11</sub> | DMU <sub>12</sub> | DMU <sub>13</sub> | DMU <sub>14</sub> | DMU <sub>15</sub> | DMU <sub>16</sub> | DMU <sub>17</sub> | DMU <sub>18</sub> |
|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| DMU <sub>1</sub>  | 2.8486           | 3.4261           | 12.5140          | 0.2102           | 2.0029           | 0.2184           | 0.4194           | 2.7303           | 0.2485           | 3.1421            | 5.1566            | 1.7693            | 20.4629           | 6.2866            | 2.4366            | 0.3464            | 0.1315            |                   |
| DMU <sub>2</sub>  | 0.1356           | 0.4645           | 1.6967           | 0.0285           | 0.2716           | 0.0296           | 0.0569           | 0.3702           | 0.0337           | 0.4260            | 0.6991            | 0.2399            | 2.7744            | 0.8523            | 0.3304            | 0.0470            | 0.0178            |                   |
| DMU <sub>3</sub>  | 15.6416          | 0.7303           | 1.5348           | 0.0485           | 0.0426           | 0.0713           | 0.0369           | 0.0378           | 20.1395          | 14.4550           | 0.1143            | 0.2557            | 0.7432            | 0.0291            | 3.8735            | 0.0346            | 0.0198            |                   |
| DMU <sub>4</sub>  | 0.0803           | 0.2288           | 0.2752           | 0.0169           | 0.1609           | 0.0175           | 0.0337           | 0.2193           | 0.0200           | 0.2524            | 0.4142            | 0.1421            | 1.6438            | 0.5050            | 0.1957            | 0.0278            | 0.0106            |                   |
| DMU <sub>5</sub>  | 0.1249           | 0.3561           | 1.5644           | 0.0169           | 0.2504           | 0.0273           | 0.0524           | 0.3413           | 0.0311           | 0.3928            | 0.6446            | 0.2212            | 2.5581            | 0.7859            | 0.3046            | 0.0433            | 0.0164            |                   |
| DMU <sub>6</sub>  | 35.9422          | 1.6782           | 3.5267           | 0.1115           | 0.1639           | 0.0848           | 0.0868           | 0.0868           | 46.2778          | 33.2155           | 0.2627            | 0.5875            | 1.7079            | 0.0669            | 8.9007            | 0.0794            | 0.0455            |                   |
| DMU <sub>7</sub>  | 0.1537           | 0.4383           | 0.5272           | 0.0323           | 0.3082           | 0.0645           | 0.0645           | 0.4201           | 0.0382           | 0.4835            | 0.7935            | 0.2723            | 3.1487            | 0.9673            | 0.3749            | 0.0533            | 0.0202            |                   |
| DMU <sub>8</sub>  | 12.8579          | 0.6004           | 0.1812           | 0.0399           | 0.0350           | 0.0586           | 0.0311           | 0.0311           | 16.5554          | 11.8825           | 0.0940            | 0.2102            | 0.6110            | 0.0240            | 3.1841            | 0.0284            | 0.0163            |                   |
| DMU <sub>9</sub>  | 55.2423          | 2.5794           | 0.7783           | 0.1713           | 0.1504           | 0.2519           | 0.1303           | 10.9617          | 71.1279          | 51.0515           | 0.4038            | 0.9029            | 2.6249            | 0.1029            | 13.6802           | 0.1221            | 0.0700            |                   |
| DMU <sub>10</sub> | 4.0109           | 11.4366          | 13.7551          | 0.8438           | 8.0413           | 0.8770           | 1.6839           | 10.9617          | 12.6148          | 20.7025           | 7.1035            | 82.1543           | 25.2393           | 9.7825            | 1.3907            | 0.5281            |                   |                   |
| DMU <sub>11</sub> | 0.3139           | 0.8949           | 1.0764           | 0.0660           | 0.6292           | 0.0686           | 0.1318           | 0.8578           | 0.0781           | 1.6200            | 0.5559            | 6.4288            | 1.9750            | 0.7655            | 0.1088            | 0.0413            |                   |                   |
| DMU <sub>12</sub> | 34.4788          | 1.6099           | 0.4858           | 0.1069           | 0.0939           | 0.1572           | 0.0813           | 0.0833           | 44.3936          | 31.8631           | 0.5636            | 1.6383            | 0.0642            | 8.5383            | 0.0762            | 0.0437            |                   |                   |
| DMU <sub>13</sub> | 0.0902           | 0.2572           | 0.3094           | 0.0190           | 0.1809           | 0.0197           | 0.0379           | 0.2466           | 0.0224           | 0.2837            | 0.4656            | 1.8478            | 0.5677            | 0.2200            | 0.0313            | 0.0119            |                   |                   |
| DMU <sub>14</sub> | 21.0451          | 0.9826           | 0.2965           | 0.0653           | 0.0573           | 0.0959           | 0.0496           | 0.0508           | 27.0969          | 19.4486           | 0.1538            | 0.3440            | 0.0392            | 5.2116            | 0.0465            | 0.0267            |                   |                   |
| DMU <sub>15</sub> | 164.9385         | 7.7013           | 2.3238           | 0.5115           | 0.4492           | 0.7520           | 0.3889           | 0.3984           | 212.3688         | 152.4260          | 1.2055            | 2.6960            | 7.8374            | 40.8455           | 0.3646            | 0.2090            |                   |                   |
| DMU <sub>16</sub> | 0.2745           | 0.7826           | 0.9412           | 0.0577           | 0.5502           | 0.0600           | 0.1152           | 0.7501           | 0.0683           | 0.8632            | 1.4166            | 0.4861            | 5.6216            | 1.7271            | 0.0952            | 0.0361            |                   |                   |
| DMU <sub>17</sub> | 11.8033          | 0.5511           | 0.1663           | 0.0366           | 0.0321           | 0.0538           | 0.0278           | 0.0285           | 15.1975          | 10.9078           | 0.0863            | 0.1929            | 0.5609            | 0.0220            | 2.9230            | 0.0150            |                   |                   |
| DMU <sub>18</sub> | 0.0932           | 0.2658           | 0.3197           | 0.0196           | 0.1869           | 0.0204           | 0.0391           | 0.2548           | 0.0232           | 0.2932            | 0.4811            | 0.1651            | 1.9093            | 0.5866            | 0.2273            | 0.0323            |                   |                   |
| e <sub>j</sub>    | 21.0133          | 1.9966           | 1.5448           | 0.1403           | 0.7908           | 0.1731           | 0.2020           | 1.0511           | 26.6895          | 20.2354           | 2.0420            | 0.9828            | 8.4867            | 2.3436            | 5.9879            | 0.1722            | 0.0741            |                   |
| Ordinal value     | 17               | 10               | 9                | 14               | 2                | 6                | 4                | 5                | 8                | 18                | 16                | 11                | 7                 | 15                | 12                | 13                | 3                 | 1                 |

**Table 5** The anticipated improvement for polysilicon process

| Response (dB)                      | Starting condition (1) | Optimal condition (2)              |                                          |                        |                           |                   | Anticipated improvement (2)–(1)    |                                          |                        |                           |                   |
|------------------------------------|------------------------|------------------------------------|------------------------------------------|------------------------|---------------------------|-------------------|------------------------------------|------------------------------------------|------------------------|---------------------------|-------------------|
|                                    |                        | Engineering judgment (Phadke 1989) | Weighted quality loss (Tong et al. 1997) | PCA (Su and Tong 1997) | DEAR (Liao and Chen 2002) | Proposed approach | Engineering judgment (Phadke 1989) | Weighted quality loss (Tong et al. 1997) | PCA (Su and Tong 1997) | DEAR (Liao and Chen 2002) | Proposed approach |
| Thickness                          | 29.95                  | 36.79                              | 40.24                                    | 41.23                  | 41.32                     | 44.79             | 10.29                              | 11.28                                    | 11.37                  | 14.84                     |                   |
| Surface defects                    | -56.69                 | -19.84                             | -24.22                                   | -2.29                  | 1.20                      | 7.03              | 32.47                              | 54.40                                    | 57.89                  | 63.72                     |                   |
| Deposition rate                    | 34.97                  | 29.60                              | 32.44                                    | 27.21                  | 27.21                     | 25.64             | -2.53                              | -7.76                                    | -7.76                  | -9.34                     |                   |
| Total anticipated improvement (dB) |                        |                                    |                                          |                        |                           |                   | 40.23                              | 57.92                                    | 61.5                   | 69.22                     |                   |

- Step 1 The  $L_{18}(2^1 \times 3^7)$  array contains 18 experiments. Each experiment is treated as a DMU as shown in the first column of Table 1. The quality loss of thickness, calculated using Eq. (3), and surface defects are set the inputs. However, the deposition rate is set as the output for all DMUs.
- Step 2 The standard efficiency,  $E_o(o = 1, \dots, 18)$  is calculated by solving the CCR model for each DMU and also displayed in the last column of Table 1. Note that all the  $E_o$  values lie between zero and one, while the  $E_o$  value for each of DMU<sub>1</sub>, DMU<sub>4</sub>, DMU<sub>10</sub>, DMU<sub>11</sub>, and DMU<sub>14</sub> is equal to one. Thus, these DMUs are identified as CCR-efficient. This shows the weakness of the CCR model in discriminating efficient DMUs.
- Step 3 Model I is adopted to evaluate the  $v_{1j}^*$ ,  $v_{2j}^*$ , and  $u_{1j}^*$  values for each DMU<sub>j</sub>. The results are shown in the columns entitled by “Model I” in Table 3. For illustration, the values of  $v_{11}^*$ ,  $v_{21}^*$ , and  $u_{11}^*$  for DMU<sub>1</sub> of 21.6778700, 0.0, and 0.0004485, respectively, are obtained by solving model I as shown below

$$\begin{aligned}
 & \text{Max } u_{11} \cdot \sum_{j=2}^{18} y_{1j} \\
 & \quad - \left( v_{11} \cdot \sum_{j=2}^{18} x_{1j} + v_{21} \cdot \sum_{j=2}^{18} x_{2j} \right) \\
 & \text{subject to } \sum_{i=1}^2 \left( v_{i1} \cdot \sum_{j=2}^{18} x_{ij} \right) = 1 \\
 & \quad u_{11} y_{1j} - \sum_{i=1}^2 v_{i1} x_{ij} \leq \delta \\
 & \quad \quad \quad j = 2, \dots, 18 \\
 & \quad u_{11} y_{11} - \sum_{i=1}^2 v_{i1} x_{i1} = 0 \\
 & \quad u_{11}, v_{11}, v_{21} \geq 0
 \end{aligned}$$

To avoid infeasible solution, the right hand side of the second constraint is set equal or less than a scalar  $\delta$ , which is very close to zero as shown in the second column of Table 3. Similarly, the  $v_{1j}^*$ ,  $v_{2j}^*$ , and  $u_{1j}^*$  are calculated for the other 17 DMUs. The  $E_{oj}$  and  $e_j$  values are then calculated for each of the 18 DMUs. Table 4 displays the corresponding cross-efficiencies matrix.

For example, in Table 4 the cross-efficiency,  $E_{2,1}$ , of DMU<sub>1</sub> evaluated using the optimal weighing scheme of DMU<sub>2</sub> of 0.1356 is calculated as follows. In Table 1, the inputs of DMU<sub>1</sub> are calculated 0.00030

and 0.67, respectively, while the output is estimated 14.5. In Table 3, using model I of benevolent formulation, the calculated  $v_{12}^*$ ,  $v_{22}^*$ , and  $u_{12}^*$  for DMU<sub>2</sub> are 21.6637800 and 0.0, and 0.0000608, respectively. Substituting these values in Eq. (1) gives

$$E_{2,1} = (0.0000608 \times 14.5)/(21.6637800 \times 0.0003 + 0.0 \times 0.67) = 0.1356$$

In a similar manner, the  $E_{o1}$  values of DMU<sub>1</sub> are evaluated using the optimal weights of DMU<sub>3</sub> to DMU<sub>18</sub>. Using Eq. (2), the mean cross-efficiency of DMU<sub>1</sub>,  $e_1$ , is then

$$e_1 = \sum_{o=2}^{18} E_{o1}/(18 - 1) = 21.0133$$

The  $e_j$  values for DMU<sub>2</sub> to DMU<sub>18</sub> are computed similarly. Contrary to the CCR model, the  $E_{oj}$  values for some DMUs, as shown in Table 4, are greater than one; for example, the values of  $E_{3,1}$  and  $E_{6,1}$  are equal to 15.641 and 35.9422, respectively. Moreover, the DMUs identified as CCR-efficient by CCR model have unequal  $e_j$  values and thus no more equally efficient using benevolent formulation. This shows that the efficiency of benevolent formulation in increasing the discrimination among efficient DMUs.

**Step 4** The ordinal values for all  $e_j$  values are listed in the last row of Table 4, where the smallest  $e_j$  value takes an ordinal value of one, whereas the largest  $e_j$  value has an ordinal value of 18. Utilizing the ordinal values, the  $AOV_{fl}$  values are calculated for all factor levels and depicted in Fig. 1. For illustration, the  $AOV_{A1}$ , the efficiency of level 1 for factor A, is calculated as the average of the ordinal values for DMU<sub>1</sub>, DMU<sub>2</sub>, DMU<sub>3</sub>, DMU<sub>10</sub>, DMU<sub>11</sub>, and DMU<sub>12</sub>, then divided by six; numerically, the  $AOV_{A1}$  (=13.5) is obtained from  $(17 + 10 + 9 + 18 + 16 + 11)/6$ . The  $AOV_{fl}$  values for the other factor levels are obtained similarly. In Fig. 1, the factor level that maximizes the level efficiency is identified as the optimal level for that factor. Based on this, the  $A_1B_1C_1D_2E_2F_2$  is the combination of factor levels that optimizes the three responses concurrently.

**Step 5** Solving model II for each DMU, the  $v_{1j}^*$ ,  $v_{2j}^*$ , and  $u_{1j}^*$  are calculated and also listed in the columns entitled “Model II” in Table 3. For illustration, the  $v_{11}^*$ ,  $v_{21}^*$ , and  $u_{11}^*$  values for DMU<sub>1</sub> are obtained by solving the below model

$$\text{Max } u_{11} \cdot \sum_{j=2}^{18} y_{1j}$$

$$\begin{aligned} \text{subject to } & \sum_{i=1}^2 \left( v_{i1} \cdot \sum_{j=2}^{18} x_{ij} \right) = 1 \\ & u_{11}y_{1j} - \sum_{i=1}^2 v_{i1}x_{ij} \leq \delta \\ & j = 2, \dots, 18 \\ & u_{11}y_{11} - \sum_{i=1}^2 v_{i1}x_{i1} = 0 \\ & u_{11}, v_{11}, v_{21} \geq 0 \end{aligned}$$

It is noted that both models provide the same  $v_{1j}^*$ ,  $v_{2j}^*$ , and  $u_{1j}^*$  values for all DMUs. As a result, the cross-efficiency matrix corresponding to model II is similar to that in Table 4. Consequently, the  $A_1B_1C_1D_2E_2F_2$  is the combination of factor levels for optimizing the three responses concurrently using Model II. At this point, it is concluded that either model I or model II can be used for solving the multi-response problem in the Taguchi method.

**Step 6** The effectiveness of proposed approach for optimizing polysilicon process is checked as follows. The average S/N ratio each factor level is calculated for all factor levels and displayed in Table 2. Then, the anticipated improvement in each response due to setting factors at  $A_2B_1C_1D_2E_2F_2$  is calculated and listed in Table 5. In addition, the anticipated improvements gained by other approaches in previous studies, including the sum of the weighted normalized quality losses (Tong et al. 1997), PCA (Su and Tong 1997), and DEAR (Liao and Chen 2002), are also displayed in Table 5.

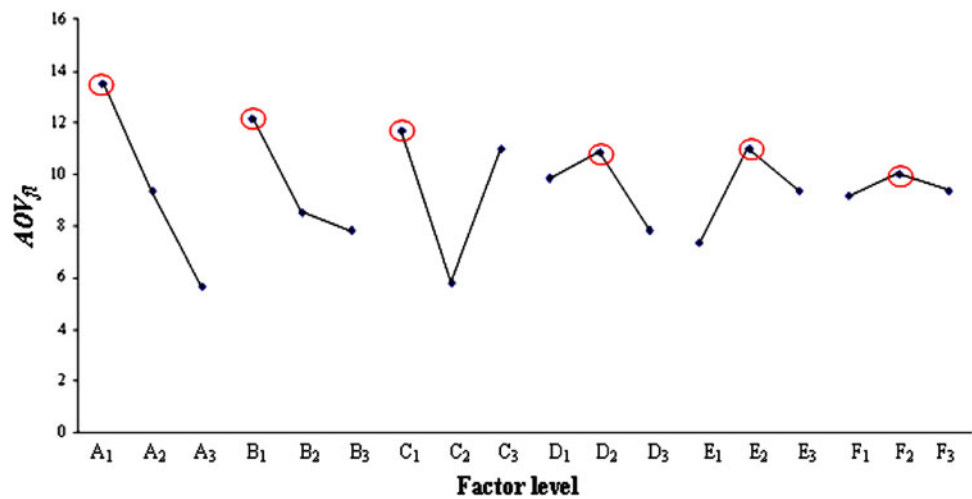
In Table 5, it is observed that the largest anticipated improvements in thickness (=14.84 dB) and surface defects (= 63.72 dB) correspond to the proposed approach. However, the largest anticipated improvement in deposition rate (= -2.53 dB) corresponds to the sum of the weighted of normalized quality losses. Nevertheless, among all techniques, the proposed approach provides the largest total anticipated improvement (= 69.22 dB). As a result, the proposed approach is superior to engineering judgment, the sum of the weighted normalized quality losses, PCA, and DEAR for solving the multiple responses problem in the Taguchi method for the polysilicon process.

### Optimizing gear hobbing operation

Jeyapaul et al. (2006) conducted genetic algorithm to optimize four STB type responses of gear hobbing operation involving: left profile (LP) error, right profile (RP) error, left helix (LH) error, and right helix (RH) error. Six



**Fig. 1** Optimal factor levels for polycilicon process



**Table 6** Experimental data of gear hobbing operation

| DMU <sub>j</sub>  | Control factor |    |   |   |   |       |                             | Inputs                      |                             |                             |       | Output (y <sub>1j</sub> ) | CCR-efficiency (E <sub>o</sub> ) |
|-------------------|----------------|----|---|---|---|-------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-------|---------------------------|----------------------------------|
|                   | A              | BC | D | E | F | Empty | LP error (x <sub>1j</sub> ) | RP error (x <sub>2j</sub> ) | LH error (x <sub>3j</sub> ) | RH error (x <sub>4j</sub> ) |       |                           |                                  |
| DMU <sub>1</sub>  | 1              | 1  | 1 | 1 | 1 | 1     | 1                           | 72.53                       | 73.97                       | 47.37                       | 42.90 | 1                         | 0.996769                         |
| DMU <sub>2</sub>  | 1              | 1  | 2 | 2 | 2 | 2     | 2                           | 75.67                       | 74.23                       | 32.43                       | 39.10 | 1                         | 1.000000                         |
| DMU <sub>3</sub>  | 1              | 1  | 3 | 3 | 3 | 3     | 3                           | 74.20                       | 73.10                       | 51.93                       | 51.10 | 1                         | 0.995628                         |
| DMU <sub>4</sub>  | 1              | 2  | 1 | 1 | 2 | 2     | 3                           | 74.80                       | 77.03                       | 61.27                       | 55.03 | 1                         | 0.960339                         |
| DMU <sub>5</sub>  | 1              | 2  | 2 | 2 | 3 | 3     | 1                           | 75.37                       | 75.93                       | 82.97                       | 59.80 | 1                         | 0.965977                         |
| DMU <sub>6</sub>  | 1              | 2  | 3 | 3 | 1 | 1     | 2                           | 71.83                       | 73.93                       | 35.83                       | 42.30 | 1                         | 1.000000                         |
| DMU <sub>7</sub>  | 1              | 3  | 1 | 2 | 1 | 3     | 2                           | 75.10                       | 71.97                       | 54.47                       | 60.07 | 1                         | 1.000000                         |
| DMU <sub>8</sub>  | 1              | 3  | 2 | 3 | 2 | 1     | 3                           | 77.03                       | 74.80                       | 56.17                       | 44.90 | 1                         | 0.972930                         |
| DMU <sub>9</sub>  | 1              | 3  | 3 | 1 | 3 | 2     | 1                           | 77.63                       | 72.27                       | 57.87                       | 59.83 | 1                         | 0.995866                         |
| DMU <sub>10</sub> | 2              | 1  | 1 | 3 | 3 | 2     | 2                           | 73.67                       | 76.80                       | 42.33                       | 47.10 | 1                         | 0.975113                         |
| DMU <sub>11</sub> | 2              | 1  | 2 | 1 | 1 | 3     | 3                           | 74.23                       | 79.03                       | 48.83                       | 34.20 | 1                         | 0.969096                         |
| DMU <sub>12</sub> | 2              | 1  | 3 | 2 | 2 | 1     | 1                           | 71.97                       | 75.37                       | 42.03                       | 30.77 | 1                         | 1.000000                         |
| DMU <sub>13</sub> | 2              | 2  | 1 | 2 | 3 | 1     | 3                           | 75.10                       | 74.53                       | 34.17                       | 34.73 | 1                         | 1.000000                         |
| DMU <sub>14</sub> | 2              | 2  | 2 | 3 | 1 | 2     | 1                           | 76.50                       | 74.50                       | 40.33                       | 37.83 | 1                         | 0.992851                         |
| DMU <sub>15</sub> | 2              | 2  | 3 | 1 | 2 | 3     | 2                           | 72.83                       | 74.77                       | 42.33                       | 40.37 | 1                         | 0.991241                         |
| DMU <sub>16</sub> | 2              | 3  | 1 | 3 | 2 | 3     | 1                           | 75.63                       | 78.73                       | 45.17                       | 35.27 | 1                         | 0.952392                         |
| DMU <sub>17</sub> | 2              | 3  | 2 | 1 | 3 | 1     | 2                           | 75.40                       | 77.07                       | 42.93                       | 39.27 | 1                         | 0.963499                         |
| DMU <sub>18</sub> | 2              | 3  | 3 | 2 | 1 | 2     | 3                           | 75.90                       | 72.00                       | 50.90                       | 47.40 | 1                         | 1.000000                         |

controllable factors were investigated including: (A) direction of hobbing, (B) number of passes, (C) source of hob, (D) feed, (E) speed, and (F) job run out. The  $L_{18}(2^1 \times 3^7)$  array was used for providing the layout of experimental work. The proposed approach was implemented for solving multi-response problem for gear hobbing operation and described as follows. Each experiment is treated as a DMU with the LP error, RP error, LH error, and RH, are set as the inputs, whereas one is set as the output for all DMUs as shown in Table 6. By solving the CCR model for each DMU, the  $E_o$  values are obtained and also displayed in Table 6. Based on the weighing scheme of the CCR model, the  $E_o$  value is

equal to one for DMU<sub>2</sub>, DMU<sub>6</sub>, DMU<sub>7</sub>, DMU<sub>12</sub>, DMU<sub>13</sub>, and DMU<sub>18</sub>, and thus these DMUs are considered equally CCR-efficient DMUs. Here also, the CCR model fails to discriminate among these efficient DMUs.

Benevolent formulation models are individually applied to measure performance for each of the 18 DMUs. The optimal input and output weights of each DMU are displayed in Table 7. It is found that both models provide the same weighing scheme for each DMU.

Utilizing the  $E_o$  values listed in Table 6 and the optimal input and outputs weights displayed in Table 7, the

**Table 7** The optimal weighing scheme by benevolent formulation for gear hobbing operation

| DMU <sub>j</sub>  | $\delta$   | Optimal input weights |            |            |            | Optimal input weight |
|-------------------|------------|-----------------------|------------|------------|------------|----------------------|
|                   |            | $v_{1j}^*$            | $v_{2j}^*$ | $v_{3j}^*$ | $v_{4j}^*$ |                      |
| DMU <sub>1</sub>  | 0.00138003 | 0.00000000            | 0.00078366 | 0.00000000 | 0.00000000 | 0.05778020           |
| DMU <sub>2</sub>  | 0.00302429 | 0.00078758            | 0.00000000 | 0.00000000 | 0.00000000 | 0.05959582           |
| DMU <sub>3</sub>  | 0.02677772 | 0.00000000            | 0.00000000 | 0.00000000 | 0.00133179 | 0.06775685           |
| DMU <sub>4</sub>  | 0.03268316 | 0.00000000            | 0.00000000 | 0.00123753 | 0.00000000 | 0.07281632           |
| DMU <sub>5</sub>  | 0.06068102 | 0.00000000            | 0.00000000 | 0.00127168 | 0.00000000 | 0.10192170           |
| DMU <sub>6</sub>  | 0.00153593 | 0.00000000            | 0.00078364 | 0.00000000 | 0.00000000 | 0.05793433           |
| DMU <sub>7</sub>  | 0.03949319 | 0.00000000            | 0.00000000 | 0.00000000 | 0.00134789 | 0.08096779           |
| DMU <sub>8</sub>  | 0.02732483 | 0.00000000            | 0.00000000 | 0.00122977 | 0.00000000 | 0.06720628           |
| DMU <sub>9</sub>  | 0.03882377 | 0.00000000            | 0.00000000 | 0.00000000 | 0.00134746 | 0.08028495           |
| DMU <sub>10</sub> | 0.02008005 | 0.00000000            | 0.00000000 | 0.00000000 | 0.00132473 | 0.06084204           |
| DMU <sub>11</sub> | 0.00363307 | 0.00000000            | 0.00078678 | 0.00000000 | 0.00000000 | 0.06025777           |
| DMU <sub>12</sub> | 0.00266738 | 0.00000000            | 0.00078452 | 0.00000000 | 0.00000000 | 0.05912949           |
| DMU <sub>13</sub> | 0.00257422 | 0.00078722            | 0.00000000 | 0.00000000 | 0.00000000 | 0.05912036           |
| DMU <sub>14</sub> | 0.00324940 | 0.00078809            | 0.00000000 | 0.00000000 | 0.00000000 | 0.05985793           |
| DMU <sub>15</sub> | 0.00168210 | 0.00000000            | 0.00078415 | 0.00000000 | 0.00000000 | 0.05811765           |
| DMU <sub>16</sub> | 0.00236911 | 0.00000000            | 0.00078660 | 0.00000000 | 0.00000000 | 0.05898046           |
| DMU <sub>17</sub> | 0.00179647 | 0.00000000            | 0.00078557 | 0.00000000 | 0.00000000 | 0.05833399           |
| DMU <sub>18</sub> | 0.02203904 | 0.00000000            | 0.00000000 | 0.00000000 | 0.00132526 | 0.06281723           |

cross-efficiencies matrix for gear hobbing operation is constructed and shown in Table 8 for both benevolent formulation models.

In order to identify the optimal combination of factor levels, the AOV<sub>f<sub>l</sub></sub> values are calculated and plotted in Fig. 2. In this figure, it is noted that the combination of optimal factor levels can be either A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>2</sub>E<sub>2</sub>F<sub>2</sub> or A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>2</sub>F<sub>2</sub>, since the optimal level for factor D can be either D<sub>2</sub> or D<sub>3</sub>. In other words, a tie occurs in selecting the level of factor D.

To decide whether to adopt A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>2</sub>E<sub>2</sub>F<sub>2</sub> or A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>2</sub>F<sub>2</sub>, the anticipated improvement in each response is calculated at A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>2</sub>E<sub>2</sub>F<sub>2</sub> and A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>2</sub>F<sub>2</sub>. The anticipated improvement gained by genetic approach (Jeyapaul et al. 2006) is also displayed in Table 9.

From Table 9, two main conclusions are obtained. First, the total anticipated improvement (= 11.2506 dB), due to setting factor levels at A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>2</sub>F<sub>2</sub>, are slightly larger than total anticipated improvement (= 10.6588 dB) due to setting factor levels at A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>2</sub>E<sub>2</sub>F<sub>2</sub>. As a result, A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>2</sub>F<sub>2</sub> is the optimal combination of factor levels. Secondly, setting factor levels at either combination provides much larger total anticipated improvement than genetic algorithm (= 4.1498 dB). Consequently, the proposed approach is concluded more effective than genetic algorithm for solving multi-response problem in the Taguchi method for the gear hobbing operation.

### Optimizing hard disk drive

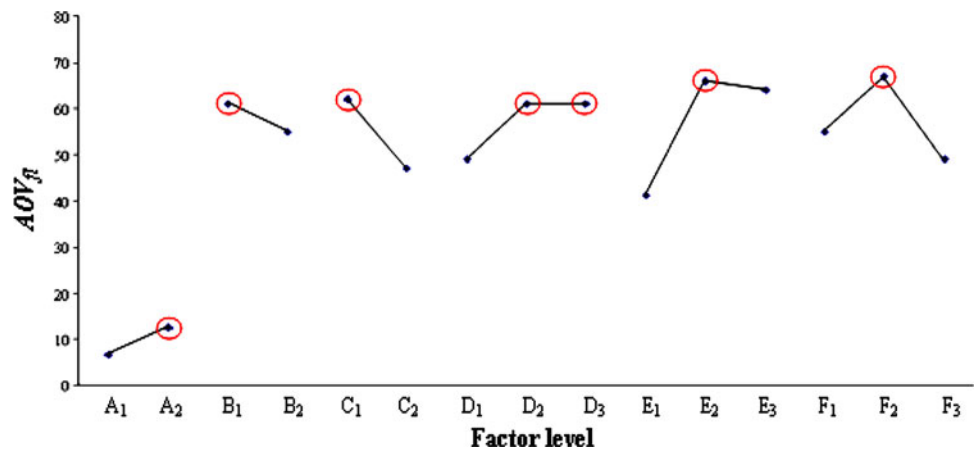
This case study was performed by the Industrial Technology Research Institute in Taiwan to improve the quality of hard disk drive. The 50% pulse width (PW), peak shift (PS), over write (OW), and high-frequency amplitude (HFA) were the four responses of main interest. The PW and PS are STB type responses, whereas OW and HFA are LTB type responses. Five controllable process factors were investigated, involving: (A) disk writability, (B) magnetization width, (C) gap length, (D) coercivity of media, and (E) rotational speed. The L<sub>18</sub> (2<sup>1</sup> × 3<sup>7</sup>) array was utilized to investigate these factors simultaneously. It was noticed that the OW has negative values with the desired target zero; however the response should be nonnegative (Phadke 1989). Since maximizing a quality response is equivalent to minimizing the negative of that response, the OW is multiplied by minus one and treated as STB type response. Let OW' equals -1 × OW. For this case study, consequently, three STB type responses and one LTB type response will be optimized concurrently as shown in Table 10.

The proposed approach is applied to optimize the four responses of hard disk drive as follows. Each experiment is treated as a DMU with the PW, PS, and OW' are set as the inputs, whereas the HFA is set as the output for all DMUs. The E<sub>o</sub> values are calculated by solving the CCR model for each DMU and also shown in Table 10. It is noted

**Table 8** The cross-efficiencies matrix for gear hobbing operation

| DMU <sub>o</sub>     | DMU <sub>j</sub> |                  |                  |                  |                  |                  |                  |                  |                  |                   |                   |                   |                   |                   |                   |                   |                   |                   |        |
|----------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|--------|
|                      | DMU <sub>1</sub> | DMU <sub>2</sub> | DMU <sub>3</sub> | DMU <sub>4</sub> | DMU <sub>5</sub> | DMU <sub>6</sub> | DMU <sub>7</sub> | DMU <sub>8</sub> | DMU <sub>9</sub> | DMU <sub>10</sub> | DMU <sub>11</sub> | DMU <sub>12</sub> | DMU <sub>13</sub> | DMU <sub>14</sub> | DMU <sub>15</sub> | DMU <sub>16</sub> | DMU <sub>17</sub> | DMU <sub>18</sub> |        |
| DMU <sub>1</sub>     | 0.9932           | 1.0086           | 1.0116           | 0.9571           | 0.9710           | 0.9973           | 1.0245           | 0.9857           | 1.0203           | 0.9600            | 0.9329            | 0.9783            | 0.9892            | 0.9897            | 0.9861            | 0.9365            | 0.9567            | 1.0240            |        |
| DMU <sub>2</sub>     | 1.0432           | 1.0198           | 1.0116           | 1.0116           | 1.0040           | 1.0534           | 1.0076           | 0.9823           | 0.9747           | 1.0272            | 1.0194            | 1.0515            | 1.0076            | 0.9892            | 1.0389            | 1.0005            | 1.0036            | 0.9970            |        |
| DMU <sub>3</sub>     | 1.1859           | 1.3012           | 0.9245           | 0.8508           | 0.8508           | 1.2028           | 0.8470           | 1.1331           | 0.8503           | 1.0802            | 1.4876            | 1.6536            | 1.4648            | 1.3448            | 1.2604            | 1.4426            | 1.2957            | 1.0733            |        |
| DMU <sub>4</sub>     | 1.2422           | 1.8142           | 1.1330           | 1.3082           | 0.7092           | 1.6420           | 1.0803           | 1.0476           | 1.0168           | 1.3899            | 1.2049            | 1.3998            | 1.7221            | 1.4588            | 1.3899            | 1.3027            | 1.3705            | 1.1560            |        |
| DMU <sub>5</sub>     | 1.6921           | 2.4711           | 1.5433           | 1.3082           | 2.2367           | 1.4715           | 1.4270           | 1.4270           | 1.3850           | 1.8932            | 1.6412            | 1.9068            | 2.3458            | 1.9871            | 1.8932            | 1.7745            | 1.8668            | 1.5746            |        |
| DMU <sub>6</sub>     | 0.9995           | 0.9959           | 1.0114           | 0.9597           | 0.9736           | 1.0273           | 0.9884           | 0.9884           | 1.0230           | 0.9626            | 0.9354            | 0.9809            | 0.9919            | 0.9923            | 0.9888            | 0.9390            | 0.9593            | 1.0268            |        |
| DMU <sub>7</sub>     | 1.4002           | 1.5363           | 1.1755           | 1.0915           | 1.0045           | 1.4201           | 1.3379           | 1.0040           | 1.0040           | 1.2754            | 1.7564            | 1.9524            | 1.7295            | 1.5878            | 1.4881            | 1.7033            | 1.5298            | 1.2673            |        |
| DMU <sub>8</sub>     | 1.1538           | 1.6850           | 1.0523           | 0.8920           | 0.6587           | 1.5251           | 1.0034           | 0.9444           | 1.2909           | 1.1191            | 1.1191            | 1.3001            | 1.5995            | 1.3549            | 1.2909            | 1.2100            | 1.2729            | 1.0737            |        |
| DMU <sub>9</sub>     | 1.3889           | 1.5239           | 1.1660           | 1.0827           | 0.9964           | 1.4086           | 0.9919           | 1.3270           | 1.2650           | 1.7422            | 1.9366            | 1.7154            | 1.5749            | 1.4760            | 1.6895            | 1.5174            | 1.2570            | 1.0737            |        |
| DMU <sub>10</sub>    | 1.0706           | 1.1746           | 0.8988           | 0.8345           | 0.7680           | 1.0858           | 0.7646           | 1.0229           | 0.7676           | 1.3429            | 1.4928            | 1.3223            | 1.2140            | 1.1378            | 1.3023            | 1.1696            | 0.9689            | 0.9689            |        |
| DMU <sub>11</sub>    | 1.0354           | 1.0317           | 1.0477           | 0.9942           | 1.0086           | 1.0359           | 1.0642           | 1.0239           | 1.0598           | 0.9972            | 1.0162            | 1.0276            | 1.0280            | 1.0280            | 1.0244            | 0.9727            | 0.9938            | 1.0637            |        |
| DMU <sub>12</sub>    | 1.0190           | 1.0153           | 1.0311           | 0.9784           | 0.9926           | 1.0194           | 1.0473           | 1.0076           | 1.0429           | 0.9814            | 0.9536            | 1.0112            | 1.0117            | 1.0081            | 0.9573            | 0.9780            | 0.9780            | 1.0468            |        |
| DMU <sub>13</sub>    | 1.0354           | 0.9925           | 1.0121           | 1.0040           | 0.9965           | 1.0455           | 1.0000           | 0.9749           | 0.9674           | 1.0195            | 1.0117            | 1.0435            | 0.9817            | 1.0311            | 0.9929            | 0.9960            | 0.9895            | 0.9895            |        |
| DMU <sub>14</sub>    | 1.0471           | 1.0038           | 1.0236           | 1.0154           | 1.0078           | 1.0574           | 1.0114           | 0.9860           | 0.9784           | 1.0310            | 1.0232            | 1.0554            | 1.0114            | 1.0428            | 1.0042            | 1.0073            | 1.0007            | 1.0007            |        |
| DMU <sub>15</sub>    | 1.0020           | 0.9984           | 1.0139           | 0.9621           | 0.9761           | 1.0025           | 1.0299           | 0.9908           | 1.0256           | 0.9650            | 0.9378            | 0.9834            | 0.9944            | 0.9948            | 0.9413            | 0.9617            | 1.0294            | 1.0294            |        |
| DMU <sub>16</sub>    | 1.0137           | 1.0101           | 1.0257           | 0.9734           | 0.9875           | 1.0142           | 1.0419           | 1.0024           | 1.0376           | 0.9763            | 0.9487            | 0.9949            | 1.0060            | 1.0065            | 1.0029            | 0.9729            | 1.0414            | 1.0414            |        |
| DMU <sub>17</sub>    | 1.0039           | 1.0003           | 1.0158           | 0.9640           | 0.9779           | 1.0044           | 1.0318           | 0.9927           | 1.0275           | 0.9669            | 0.9396            | 0.9853            | 0.9963            | 0.9967            | 0.9932            | 0.9431            | 1.0313            | 1.0313            |        |
| DMU <sub>18</sub>    | 1.1049           | 1.2123           | 0.9276           | 0.8613           | 0.7926           | 1.1206           | 0.7891           | 1.0557           | 0.7922           | 1.0064            | 1.3860            | 1.5406            | 1.3647            | 1.2529            | 1.1742            | 1.3440            | 1.2071            | 1.2071            |        |
| <i>e<sub>j</sub></i> | 1.1434           | 2.4178           | 2.0118           | 1.8683           | 1.7417           | 2.3190           | 1.9148           | 2.0318           | 1.8797           | 2.1209            | 2.2647            | 2.4747            | 2.4777            | 2.3073            | 2.2474            | 2.2730            | 2.2288            | 2.0691            | 2.0691 |
| Ordinal value        | 1                | 16               | 6                | 3                | 2                | 15               | 5                | 7                | 4                | 9                 | 12                | 17                | 18                | 14                | 11                | 13                | 10                | 8                 | 8      |

**Fig. 2** Optimal factor levels for gear hobbing operation



**Table 9** Summary of anticipated improvement for gear hobbing operation

| Response (dB)                      | Initial condition (1) | Optimal condition (2)                                                                     |                                                                                           |                                                                                           |                                                                                           | Anticipated improvement (2)–(1)                                                           |                                                                                           |                   |
|------------------------------------|-----------------------|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-------------------|
|                                    |                       | Genetic algorithm (Jeyapaul et al. 2006)                                                  |                                                                                           | Proposed approach                                                                         |                                                                                           | Genetic algorithm (Jeyapaul et al. 2006)                                                  |                                                                                           | Proposed approach |
|                                    |                       | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>2</sub> E <sub>2</sub> F <sub>2</sub> | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>3</sub> E <sub>2</sub> F <sub>2</sub> | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>2</sub> E <sub>2</sub> F <sub>2</sub> | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>3</sub> E <sub>2</sub> F <sub>2</sub> | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>2</sub> E <sub>2</sub> F <sub>2</sub> | A <sub>2</sub> B <sub>1</sub> C <sub>1</sub> D <sub>3</sub> E <sub>2</sub> F <sub>2</sub> |                   |
| LP error                           | –37.8581              | –37.4917                                                                                  | –37.3728                                                                                  | –37.1800                                                                                  | 0.3664                                                                                    | 0.4853                                                                                    | 0.6781                                                                                    |                   |
| RP error                           | –37.4952              | –37.4045                                                                                  | –37.7724                                                                                  | –37.4984                                                                                  | 0.0907                                                                                    | –0.2772                                                                                   | –0.0032                                                                                   |                   |
| LH error                           | –36.6009              | –34.4082                                                                                  | –31.9040                                                                                  | –31.4320                                                                                  | 2.1927                                                                                    | 4.6968                                                                                    | 5.1688                                                                                    |                   |
| RH error                           | –35.7397              | –34.2396                                                                                  | –29.9858                                                                                  | –30.3328                                                                                  | 1.5001                                                                                    | 5.7539                                                                                    | 5.4069                                                                                    |                   |
| Total anticipated improvement (dB) |                       |                                                                                           |                                                                                           |                                                                                           | 4.1498                                                                                    | 10.6588                                                                                   | 11.2506                                                                                   |                   |

**Table 10** Experimental data of hard disk drive

| DMU <sub>j</sub>  | Control factors |   |   |   |   |       |   | Input                 |                       |                        | Output                 | CCR-efficiency (E <sub>o</sub> ) |
|-------------------|-----------------|---|---|---|---|-------|---|-----------------------|-----------------------|------------------------|------------------------|----------------------------------|
|                   | A               | B | C | D | E | Empty |   | PW (x <sub>1j</sub> ) | PS (x <sub>2j</sub> ) | OW' (x <sub>3j</sub> ) | HFA (y <sub>1j</sub> ) |                                  |
| DMU <sub>1</sub>  | 1               | 1 | 1 | 1 | 1 | 1     | 1 | 64.75                 | 11.45                 | 31.15                  | 272.15                 | 0.60996                          |
| DMU <sub>2</sub>  | 1               | 1 | 2 | 2 | 2 | 2     | 2 | 65.10                 | 12.30                 | 34.05                  | 326.80                 | 0.68183                          |
| DMU <sub>3</sub>  | 1               | 1 | 3 | 3 | 3 | 3     | 3 | 66.30                 | 14.15                 | 35.75                  | 367.75                 | 0.66695                          |
| DMU <sub>4</sub>  | 1               | 2 | 1 | 1 | 2 | 2     | 3 | 55.55                 | 10.00                 | 32.50                  | 311.75                 | 0.80002                          |
| DMU <sub>5</sub>  | 1               | 2 | 2 | 2 | 3 | 3     | 1 | 57.00                 | 10.70                 | 35.55                  | 350.65                 | 0.84098                          |
| DMU <sub>6</sub>  | 1               | 2 | 3 | 3 | 1 | 1     | 2 | 88.40                 | 18.45                 | 39.20                  | 223.90                 | 0.31422                          |
| DMU <sub>7</sub>  | 1               | 3 | 1 | 2 | 1 | 3     | 2 | 64.85                 | 10.95                 | 30.60                  | 273.60                 | 0.64121                          |
| DMU <sub>8</sub>  | 1               | 3 | 2 | 3 | 2 | 1     | 3 | 65.20                 | 11.40                 | 34.55                  | 320.35                 | 0.72113                          |
| DMU <sub>9</sub>  | 1               | 3 | 3 | 1 | 3 | 2     | 1 | 66.25                 | 14.90                 | 45.10                  | 297.75                 | 0.51859                          |
| DMU <sub>10</sub> | 2               | 1 | 1 | 3 | 3 | 2     | 2 | 48.60                 | 11.40                 | 18.95                  | 422.40                 | 1.00000                          |
| DMU <sub>11</sub> | 2               | 1 | 2 | 1 | 1 | 3     | 3 | 75.95                 | 17.10                 | 33.10                  | 277.30                 | 0.42697                          |
| DMU <sub>12</sub> | 2               | 1 | 3 | 2 | 2 | 1     | 1 | 75.70                 | 17.75                 | 34.45                  | 329.60                 | 0.50097                          |
| DMU <sub>13</sub> | 2               | 2 | 1 | 2 | 3 | 1     | 3 | 48.60                 | 10.80                 | 24.05                  | 420.85                 | 1.00000                          |
| DMU <sub>14</sub> | 2               | 2 | 2 | 3 | 1 | 2     | 1 | 76.00                 | 15.55                 | 29.30                  | 296.65                 | 0.50461                          |
| DMU <sub>15</sub> | 2               | 2 | 3 | 1 | 2 | 3     | 2 | 75.70                 | 18.60                 | 38.65                  | 258.65                 | 0.39312                          |
| DMU <sub>16</sub> | 2               | 3 | 1 | 3 | 2 | 3     | 1 | 55.55                 | 12.50                 | 18.80                  | 360.95                 | 0.86134                          |
| DMU <sub>17</sub> | 2               | 3 | 2 | 1 | 3 | 1     | 2 | 57.00                 | 12.75                 | 35.10                  | 360.10                 | 0.72924                          |
| DMU <sub>18</sub> | 2               | 3 | 3 | 2 | 1 | 2     | 3 | 88.35                 | 20.35                 | 37.75                  | 257.60                 | 0.33589                          |

**Table 11** The optimal weighing scheme by benevolent formulation for gear hobbing operation

| DMU <sub>j</sub>  | δ          | Optimal input weights |            |            | Optimal output weights |
|-------------------|------------|-----------------------|------------|------------|------------------------|
|                   |            | $v_{1j}^*$            | $v_{2j}^*$ | $v_{3j}^*$ | $u_{4j}^*$             |
| DMU <sub>1</sub>  | 0.01123747 | 0.00088488            | 0.00000000 | 0.00000000 | 0.00012842             |
| DMU <sub>2</sub>  | 0.01994025 | 0.00000000            | 0.00000000 | 0.00180326 | 0.00012811             |
| DMU <sub>3</sub>  | 0.01526047 | 0.00000000            | 0.00000000 | 0.00180881 | 0.00011728             |
| DMU <sub>4</sub>  | 0.02927371 | 0.00000000            | 0.00000000 | 0.00179824 | 0.00014998             |
| DMU <sub>5</sub>  | 0.03085495 | 0.00000000            | 0.00000000 | 0.00180816 | 0.00015417             |
| DMU <sub>6</sub>  | 0.00343709 | 0.00090379            | 0.00000000 | 0.00000000 | 0.00011212             |
| DMU <sub>7</sub>  | 0.01380309 | 0.00088496            | 0.00000000 | 0.00000000 | 0.00013450             |
| DMU <sub>8</sub>  | 0.02509146 | 0.00000000            | 0.00000000 | 0.00180489 | 0.00014037             |
| DMU <sub>9</sub>  | 0.02618165 | 0.00000000            | 0.00000000 | 0.00183993 | 0.00014453             |
| DMU <sub>10</sub> | 0.00232861 | 0.00000000            | 0.00417188 | 0.00000000 | 0.00011259             |
| DMU <sub>11</sub> | 0.00119998 | 0.00000000            | 0.00427350 | 0.00000000 | 0.00011252             |
| DMU <sub>12</sub> | 0.00237426 | 0.00000000            | 0.00428541 | 0.00000000 | 0.00011562             |
| DMU <sub>13</sub> | 0.00000000 | 0.00000000            | 0.00416147 | 0.00000000 | 0.00010679             |
| DMU <sub>14</sub> | 0.00536898 | 0.00089377            | 0.00000000 | 0.00000000 | 0.00011555             |
| DMU <sub>15</sub> | 0.00472010 | 0.00000000            | 0.00430108 | 0.00000000 | 0.00012159             |
| DMU <sub>16</sub> | 0.00734913 | 0.00000000            | 0.00419112 | 0.00000000 | 0.00012502             |
| DMU <sub>17</sub> | 0.02000846 | 0.00000000            | 0.00000000 | 0.00180669 | 0.00012842             |
| DMU <sub>18</sub> | 0.00159118 | 0.00000000            | 0.00433369 | 0.00000000 | 0.00011499             |

that DMU<sub>10</sub> and DMU<sub>13</sub> are the only CCR-efficient DMUs. Utilizing the  $E_o$  values, benevolent formulation models are solved separately to estimate the optimal input and output weights of each of the 18 DMUs as shown in Table 11 for both models.

Since both models provide the same weighing scheme for each DMU, the cross-efficiencies matrix for hard disk drive shown in Table 12 corresponds to both models. As a result, both models provide the same combination of optimal factor levels for multi-responses.

Utilizing the ordinal values in Table 12, the AOV<sub>f1</sub> values are calculated for each factor level and depicted in Fig. 3. Obviously, the combination of optimal factor levels is identified as A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>3</sub>. The anticipated improvement in each response due to setting factor levels at A<sub>2</sub>B<sub>1</sub>C<sub>1</sub>D<sub>3</sub>E<sub>3</sub> is calculated and compared with the anticipated improvement using PCA (Su and Tong 1997) and DEAR (Liao and Chen 2002) in Table 13.

In Table 13, the total anticipated improvement gained by the proposed approach is 10.681 dB. Whereas, the total anticipated improvement using PCA and DEAR are 2.61 and 3.35 dB, respectively. Obviously, the proposed approach outperforms PCA and DEAR in solving the multi-response problem in the Taguchi method for hard disk drive.

### Conclusions

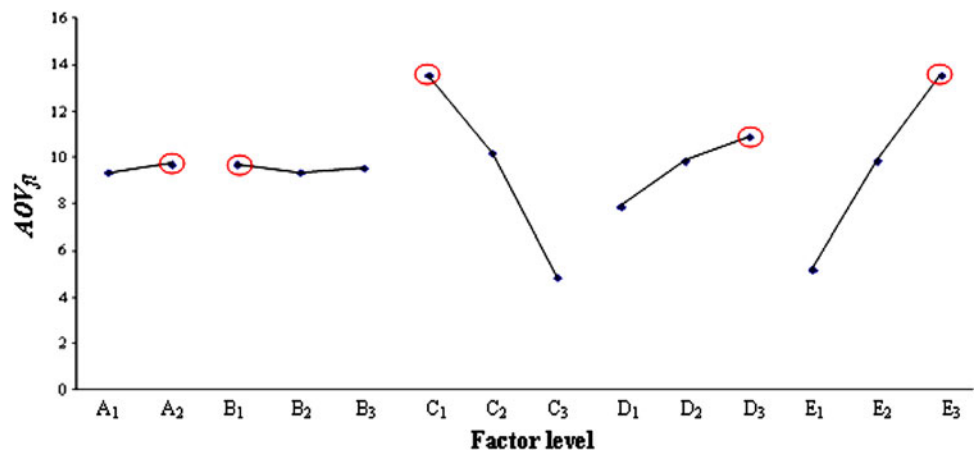
This research proposes an approach for solving the multi-response problem in the Taguchi method utilizing benevolent formulation in DEA. Three case studies are provided for illustration. From the computational results of three case studies, the following advantages of the proposed approach are noted regarding:

- *Efficiency*: The proposed approach is found the most efficient in solving the multi-response problem in the Taguchi method, as it provides the largest anticipated improvement for all the three cases.
- *Priori information*: In contrast to the Taguchi method and weighted S/N ratios method, the proposed approach does not require any priori information about response weights or importance.
- *Discrimination*: Opposite to CCR-model, the benevolent technique increases discrimination among efficient DMUs.
- *Assumption*: The proposed approach is not based on rigid assumptions, whereas PCA does.
- *Simplicity*: Contrary to GA, neural networks, grey analysis, and regression method, the proposed approach can be easily understood and implemented by practitioners.

**Table 12** The cross-efficiencies matrix for hard disk drive

| DMU <sub>i</sub>  | DMU <sub>1</sub> | DMU <sub>2</sub> | DMU <sub>3</sub> | DMU <sub>4</sub> | DMU <sub>5</sub> | DMU <sub>6</sub> | DMU <sub>7</sub> | DMU <sub>8</sub> | DMU <sub>9</sub> | DMU <sub>10</sub> | DMU <sub>11</sub> | DMU <sub>12</sub> | DMU <sub>13</sub> | DMU <sub>14</sub> | DMU <sub>15</sub> | DMU <sub>16</sub> | DMU <sub>17</sub> | DMU <sub>18</sub> |
|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| DMU <sub>1</sub>  | 0.72851          | 0.80496          | 0.81443          | 0.89275          | 0.36757          | 0.61226          | 0.71303          | 0.65223          | 1.26131          | 0.52985           | 0.63186           | 1.25668           | 0.56645           | 0.49585           | 0.94297           | 0.91681           | 0.42313           |                   |
| DMU <sub>2</sub>  | 0.62067          | 0.73078          | 0.68145          | 0.70072          | 0.40577          | 0.63519          | 0.6587           | 0.46901          | 1.58353          | 0.59516           | 0.67969           | 1.24315           | 0.71926           | 0.47542           | 1.36396           | 0.72883           | 0.48477           |                   |
| DMU <sub>3</sub>  | 0.56646          | 0.62227          | 0.62193          | 0.63951          | 0.37033          | 0.57971          | 0.60116          | 0.42805          | 1.44521          | 0.54317           | 0.62032           | 1.13456           | 0.65644           | 0.43389           | 1.24482           | 0.66517           | 0.44243           |                   |
| DMU <sub>4</sub>  | 0.72867          | 0.80047          | 0.85794          | 0.82264          | 0.47637          | 0.74571          | 0.77331          | 0.55062          | 1.85906          | 0.69871           | 0.79795           | 1.45945           | 0.84441           | 0.55814           | 1.60128           | 0.85565           | 0.56912           |                   |
| DMU <sub>5</sub>  | 0.74491          | 0.81831          | 0.87706          | 0.81785          | 0.48699          | 0.76234          | 0.79055          | 0.56289          | 1.90049          | 0.71429           | 0.81574           | 1.49198           | 0.86323           | 0.57058           | 1.63697           | 0.87472           | 0.58181           |                   |
| DMU <sub>6</sub>  | 0.52144          | 0.62278          | 0.68813          | 0.69623          | 0.76319          | 0.52341          | 0.60955          | 0.55757          | 1.07825          | 0.45295           | 0.54016           | 1.07429           | 0.48424           | 0.42389           | 0.80611           | 0.78375           | 0.36172           |                   |
| DMU <sub>7</sub>  | 0.6388           | 0.76295          | 0.84301          | 0.85294          | 0.93496          | 0.38494          | 0.74674          | 0.68306          | 1.32094          | 0.5549            | 0.66174           | 1.31609           | 0.59323           | 0.51929           | 0.98755           | 0.96016           | 0.44313           |                   |
| DMU <sub>8</sub>  | 0.6795           | 0.74645          | 0.80004          | 0.74604          | 0.76713          | 0.44423          | 0.6954           | 0.51347          | 1.73361          | 0.65157           | 0.74411           | 1.36097           | 0.78743           | 0.52048           | 1.49323           | 0.79791           | 0.53072           |                   |
| DMU <sub>9</sub>  | 0.68628          | 0.7539           | 0.80803          | 0.75348          | 0.77479          | 0.44866          | 0.70233          | 0.72833          | 1.75091          | 0.65807           | 0.75153           | 1.37455           | 0.79529           | 0.52567           | 1.50813           | 0.80587           | 0.53602           |                   |
| DMU <sub>10</sub> | 0.64148          | 0.71706          | 0.70142          | 0.84137          | 0.88445          | 0.32752          | 0.67435          | 0.7584           | 0.53932          | 0.43766           | 0.50115           | 1.05168           | 0.51487           | 0.3753            | 0.77932           | 0.76224           | 0.34164           |                   |
| DMU <sub>11</sub> | 0.62582          | 0.69955          | 0.68429          | 0.82082          | 0.86285          | 0.31952          | 0.65788          | 0.73988          | 0.52615          | 0.97558           | 0.48891           | 1.026             | 0.50229           | 0.36614           | 0.76029           | 0.74363           | 0.33329           |                   |
| DMU <sub>12</sub> | 0.64125          | 0.7168           | 0.70116          | 0.84106          | 0.88412          | 0.3274           | 0.6741           | 0.75813          | 0.53912          | 0.99964           | 0.4375            | 1.0513            | 0.51468           | 0.37516           | 0.77904           | 0.76197           | 0.34151           |                   |
| DMU <sub>13</sub> | 0.60996          | 0.68183          | 0.66695          | 0.80002          | 0.84098          | 0.31143          | 0.64121          | 0.72113          | 0.51282          | 0.95086           | 0.41615           | 0.47652           | 0.48957           | 0.35686           | 0.74103           | 0.72479           | 0.32485           |                   |
| DMU <sub>14</sub> | 0.54337          | 0.64897          | 0.71707          | 0.72552          | 0.79529          | 0.32744          | 0.54542          | 0.63519          | 0.58102          | 1.1236            | 0.47201           | 0.56288           | 1.11948           | 0.44171           | 0.84002           | 0.81672           | 0.37693           |                   |
| DMU <sub>15</sub> | 0.67194          | 0.75111          | 0.73472          | 0.88132          | 0.92644          | 0.34307          | 0.70636          | 0.79441          | 0.56493          | 1.04748           | 0.45844           | 0.52495           | 1.10161           | 0.53931           | 0.81632           | 0.79843           | 0.35785           |                   |
| DMU <sub>16</sub> | 0.70899          | 0.79253          | 0.77524          | 0.92992          | 0.97752          | 0.36199          | 0.74531          | 0.83822          | 0.59608          | 1.10524           | 0.48372           | 0.55389           | 1.16236           | 0.56905           | 0.4148            | 0.84246           | 0.37759           |                   |
| DMU <sub>17</sub> | 0.62102          | 0.68221          | 0.73119          | 0.68183          | 0.70111          | 0.406            | 0.63555          | 0.65907          | 0.46928          | 1.58442           | 0.59549           | 0.68007           | 1.24385           | 0.71967           | 0.47568           | 1.36472           | 0.48505           |                   |
| DMU <sub>18</sub> | 0.63069          | 0.70501          | 0.68962          | 0.82722          | 0.86957          | 0.32201          | 0.66301          | 0.74565          | 0.53025          | 0.98318           | 0.4303            | 0.49273           | 1.034             | 0.50621           | 0.36899           | 0.76622           | 0.74943           |                   |
| e <sub>j</sub>    | 0.64007          | 0.72063          | 0.75362          | 0.78432          | 0.82577          | 0.37831          | 0.6588           | 0.72185          | 0.54564          | 1.33549           | 0.53705           | 0.61907           | 1.206             | 0.62739           | 0.45281           | 1.08423           | 0.79933           | 0.43009           |
| Ordinal value     | 8                | 10               | 12               | 13               | 15               | 1                | 9                | 11               | 5                | 18                | 4                 | 6                 | 17                | 7                 | 3                 | 16                | 14                | 2                 |

**Fig. 3** Optimal factor levels for hard disk drive



**Table 13** Summary of anticipated improvement for hard disk drive

| Response (dB)                      | Initial condition (1) | Optimal condition (2)  |                           |                   | Anticipated improvement (2)–(1) |                           |                   |
|------------------------------------|-----------------------|------------------------|---------------------------|-------------------|---------------------------------|---------------------------|-------------------|
|                                    |                       | PCA (Su and Tong 1997) | DEAR (Liao and Chen 2002) | Proposed approach | PCA (Su and Tong 1997)          | DEAR (Liao and Chen 2002) | Proposed approach |
| PW                                 | –36.28                | –33.74                 | –33.74                    | –33.734           | 2.54                            | 2.54                      | 2.543             |
| PS                                 | –21.48                | –19.37                 | –19.17                    | –21.045           | 2.11                            | 2.31                      | 0.435             |
| OW                                 | 31.51 <sup>a</sup>    | 27.71                  | 28.97                     | –25.669           | –3.80                           | –2.54                     | 5.219             |
| HFA                                | 50.47                 | 52.23                  | 51.51                     | 52.949            | 1.76                            | 1.04                      | 2.484             |
| Total anticipated improvement (dB) |                       |                        |                           |                   | 2.61                            | 3.35                      | 10.681            |

<sup>a</sup> Initial condition is multiplied by minus one, and thus initial condition is –31.51

The above advantages may make the proposed approach be used for solving the multi-response problem for a wide range of applications in manufacturing on the Taguchi method. In conclusion, benevolent formulation is not only efficient in comparison among DMUs at organizational level, but also effective for solving the multi-response problem in manufacturing at operational level. Future research will be conducted to solve the multi-response problem in the Taguchi method with correlated multiple responses in the Taguchi method utilizing DEA techniques.

**Appendix A: CCR-model**

Assuming there are  $n$  DMUs each with  $m$  inputs and  $s$  outputs to be evaluated. Let the DMU to be individually evaluated on any trial be designated as  $DMU_o$ , where  $o$  ranges from one to  $n$ . The relative efficiency,  $E_o$ , of  $DMU_o$  with inputs of  $x_{io}$  ( $i = 1, \dots, m$ ) and outputs of  $y_{ro}$  ( $r = 1, \dots, s$ ) is evaluated by CCR model as follows:

$$E_o = \text{Max } \theta = \left( \sum_{r=1}^s u_r y_{ro} \right) / \left( \sum_{i=1}^m v_i x_{io} \right)$$

$$\text{subject to } \begin{aligned} & \left( \sum_{r=1}^s u_r y_{rj} \right) / \left( \sum_{i=1}^m v_i x_{ij} \right) \leq 1 \\ & j = 1, \dots, n \\ & u_1, u_2, \dots, u_s \geq 0 \\ & v_1, v_2, \dots, v_m \geq 0 \end{aligned}$$

where  $u_r$  and  $v_i$  are the virtual weights for the  $r$ th output and  $i$ th input, respectively, and  $\theta$  is a scalar. The objective function is the ratio of the sum of the weighted outputs relative to the sum of the weighted inputs. The first constraint ensures that  $E_j$  lies between zero and one for all the  $n$  DMUs. Obviously, the CCR model is nonlinear, which can be transformed into a linear model by setting the sum of the weighted inputs equal to one. The resulting model is called the “input-oriented” CCR model, which is expressed as follows:

$$\begin{aligned} E_o = \text{Max } \theta &= \sum_{r=1}^s u_r y_{ro} \\ \text{subject to } & \sum_{i=1}^m v_i x_{io} = 1 \\ & \sum_{r=1}^s u_r y_{rj} \leq \sum_{i=1}^m v_i x_{ij} \quad j = 1, \dots, n \end{aligned}$$

$$\begin{aligned} u_1, u_2, \dots, u_s &\geq 0 \\ v_1, v_2, \dots, v_m &\geq 0 \end{aligned}$$

$$\begin{aligned} \sum_{r=1}^s u_{ro} y_{rj} - E_o \cdot \sum_{i=1}^m v_{io} x_{ij} &= 0 \\ u_{ro}, v_{io} &\geq 0 \end{aligned}$$

## Appendix B: Benevolent formulation models

### Model I

This model is expressed as:

$$\begin{aligned} \text{Max} \quad & \sum_{r=1}^s \left( u_{ro} \cdot \sum_{j \neq o} y_{rj} \right) - \sum_{i=1}^m \left( v_{io} \cdot \sum_{j \neq o} x_{ij} \right) \\ \text{subject to} \quad & \sum_{i=1}^m \left( v_{io} \cdot \sum_{j \neq o} x_{ij} \right) = 1, \\ & \sum_{r=1}^s u_{ro} y_{rj} - \sum_{i=1}^m v_{io} x_{ij} \leq 0, \quad \forall j \neq o \\ & \sum_{r=1}^s u_{ro} y_{ro} - E_o \cdot \sum_{i=1}^m v_{io} x_{io} = 0, \\ & u_{ro}, v_{io} \geq 0, \quad \forall r, \forall i \end{aligned}$$

In this model, the decision variables are  $u_{ro}$  and  $v_{io}$ . For  $DMU_o$ , the objective function would presumably seek to maximize the other  $DMU$ 's cross-efficiencies when measuring them by applying its own best weights. The first constraint is used to transform the objective function into linear function by setting the sum of other  $(n - 1)$   $DMU$ s inputs and outputs weighted by  $DMU_o$ 's input and output weights, respectively, equal to one. The second constraint guarantees that the relative efficiency scores for all  $DMU$ s; except  $DMU_o$ , are less than one. The third constraint keeps the relative efficiency of  $DMU_o$  calculated by CCR-Model equal to  $E_o$ . The last constraint is to obtain positive optimal values for the decision variables  $v_{io}$  and  $u_{ro}$ .

### Model II

In Model II, the objective function is to maximize the sum of the weighted outputs, while the constraints are similar to Model I. Mathematically,

$$\begin{aligned} \text{Max} \quad & \sum_{r=1}^s \left( u_{ro} \cdot \sum_{j \neq o} y_{rj} \right) \\ \text{subject to} \quad & \sum_{i=1}^m \left( v_{io} \cdot \sum_{j \neq o} x_{ij} \right) = 1 \\ & \sum_{r=1}^s u_{ro} y_{rj} - \sum_{i=1}^m v_{io} x_{ij} \leq 0, \quad \forall j \neq o \end{aligned}$$

Similar to Model I, the decision variables are  $u_{ro}$  and  $v_{io}$ .

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